

CLAIMS

428 — 1. A steel wire having a diameter ranging from 0.10mm to 0.40mm obtained by subjecting a high-carbon steel wire material having a carbon content ranging from 0.70% to 0.90% in weight to heat treatment and wire drawing, characterized in;

that tensile strength TS (N/mm²) of the steel wire satisfies following formula,

$$TS \geq 2250 - 1450 \log D \quad (1)$$

wherein D is the diameter of the steel wire in mm and log means common logarithm,

and that repeated torsion value RT (turns/100D) of the steel wire, which is defined as sum of forward twisting and reverse twisting given until a crack is formed on a steel wire in a test wherein a steel wire is subjected to a repetition of forward twisting equivalent to 3 turns per 100D and reverse twisting to the original state with the axis of the steel wire kept straight, satisfies following formula.

$$\log RT \geq 2 - 0.001 \{TS - (2250 - 1450 \log D)\} \quad (2)$$

2. A steel wire according to claim 1, having tensile strength TS (N/mm²) satisfying following formula.

$$TS \geq 2750 - 1450 \log D \quad (3)$$

3. A steel wire according to claim 2, having repeated torsion value RT not less than 60% of RT of the same steel wire the surface layer of which has been removed by the amount equivalent to 10% of total volume.

4. A steel wire according to claim 1 to 3, having breaking torsion value, which is defined as an amount of twisting to one direction subjected to a steel wire until the steel wire is broken, not less than 20 turns per 100D when the steel wire has been given such a preforming that the steel wire has minimum radius of curvature of 10 to 60 times its diameter and embedded in rubber and taken out from the rubber after vulcanization.

5. A method of manufacturing a steel wire according to claim 1

comprising a step of drawing a high-carbon steel wire material after heat treatment, characterized in that the step of drawing is carried out according to following conditions;

- 50B
C2
CST/A
- ① reduction per die is set ^{from} $(22.67 \epsilon + 3)\%$ to 29% for dies at which ϵ is less than 0.75, ATP 11/20/01
- ② reduction per die is set from 20% to 29% for dies at which ϵ is not less than 0.75 and not more than 2.25,
- ③ reduction per die is set from $(-5.56 \epsilon + 32.5)\%$ to $(-6.22 \epsilon + 43)\%$ for dies at which ϵ is more than 2.25 except for the final die,
- * ④ reduction per die is set from 4% to $(-8.3 \epsilon + 40.6)\%$ for the final die, and
- ⑤ ϵ at the final die is set from 3.0 to 4.3,

wherein ϵ is drawing strain expressed by a formula $\epsilon = 2 \ln(d_0/d)$ (4), d_0 is diameter of the steel wire material in mm before drawing, d is diameter of the steel wire in mm after passing through a die, and \ln means natural logarithm.

6. A method of manufacturing a steel wire according to claim 5, wherein ϵ at the final die is set from 3.5 to 4.2.

7. A method of manufacturing a steel wire according to claim 5, wherein a bending operation with tension is applied to the steel wire drawn through the final die.

ASD 3

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